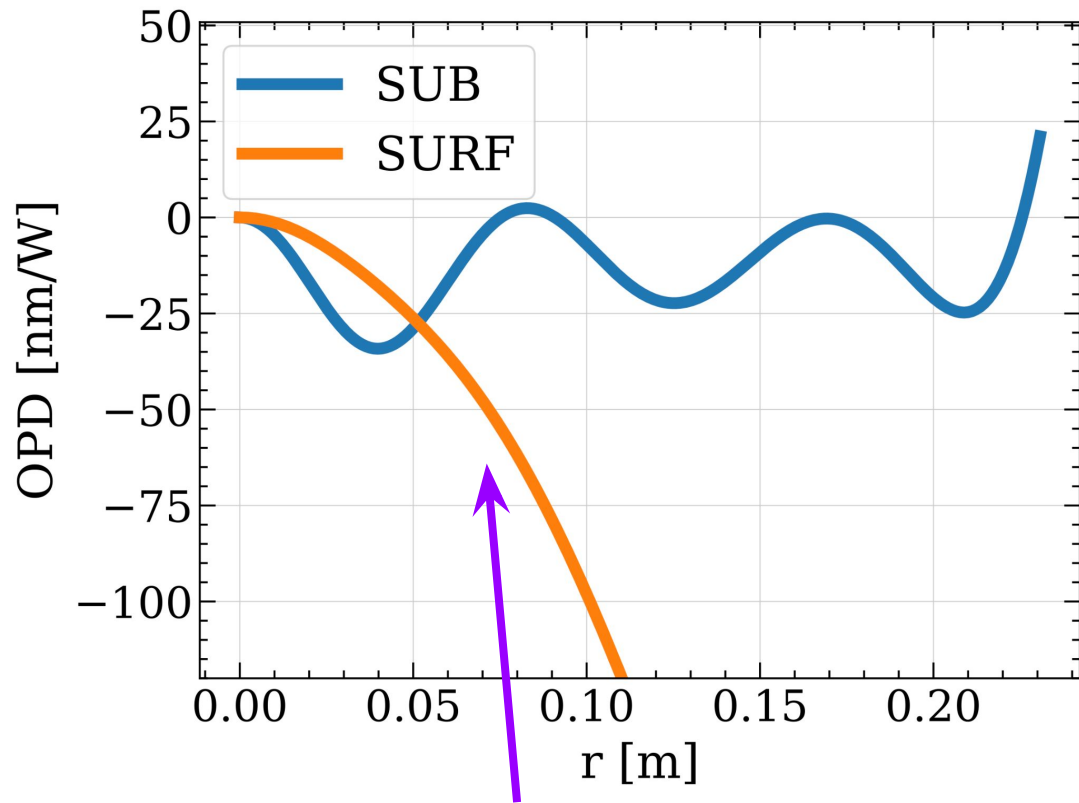


Ring Heater Quadratic Actuation

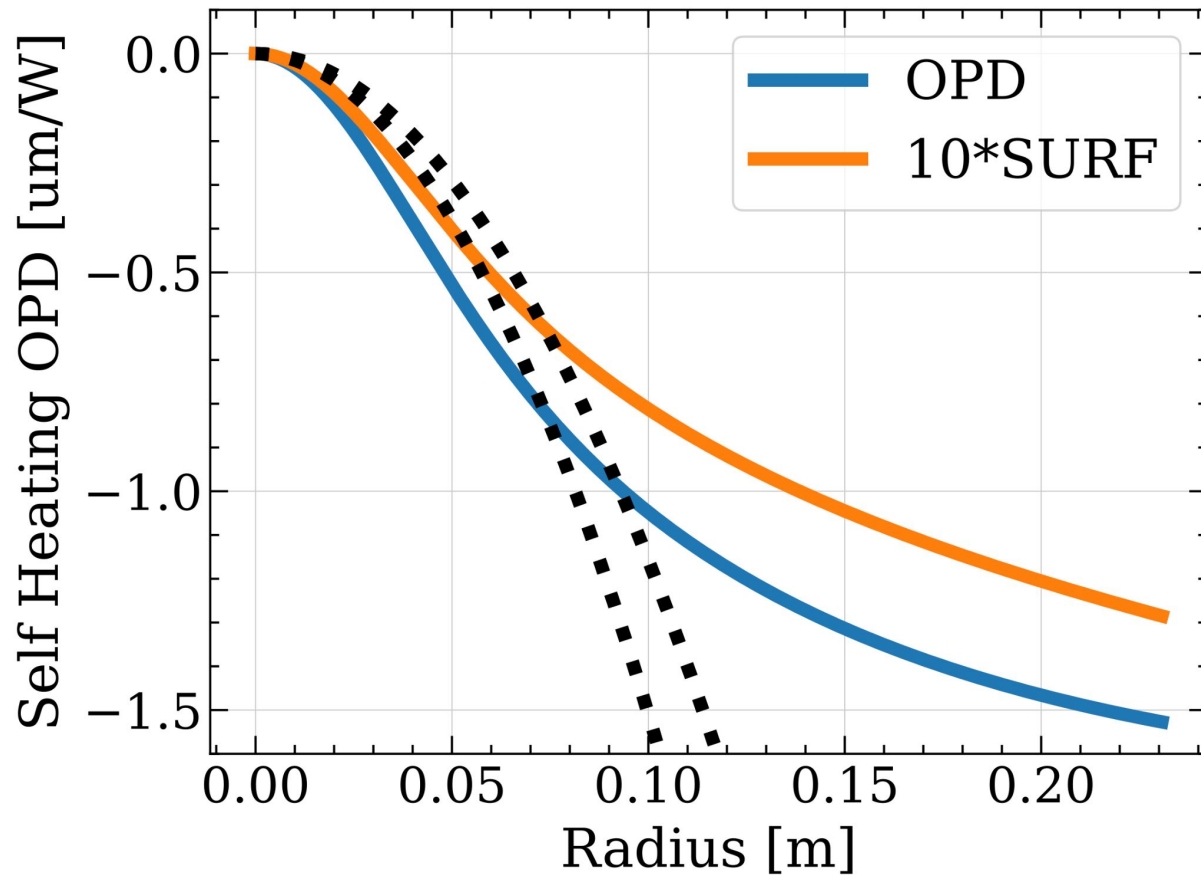


Residual quadratic deformation on the surface

Optimization results for multi-ring FROSTI with 2 heater components:

	Sub. (nm)	Surf. (nm)
2 comp.	10.3	13.6

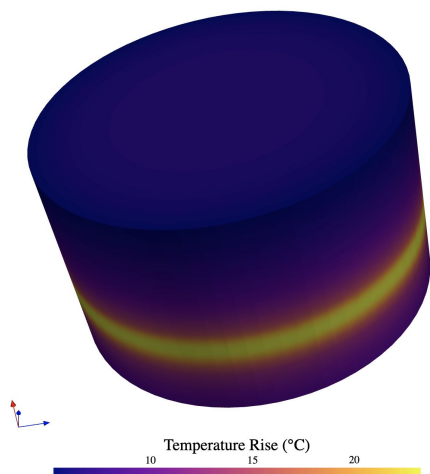
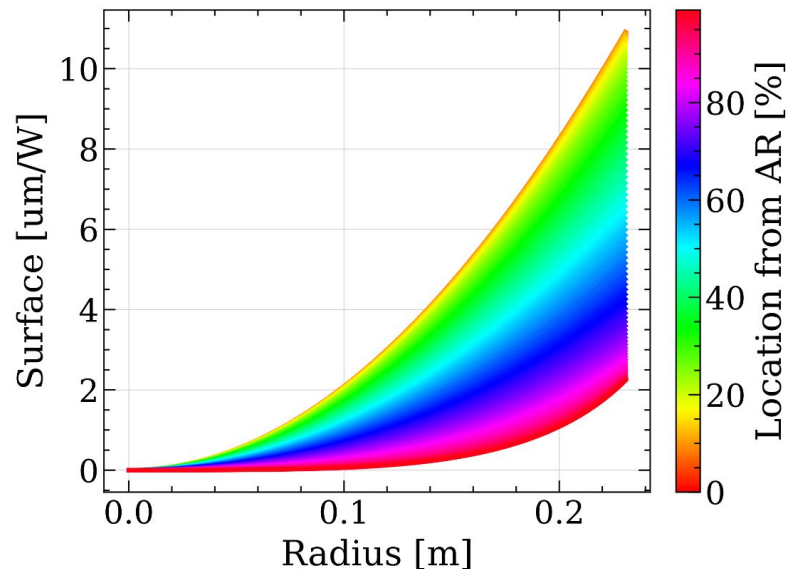
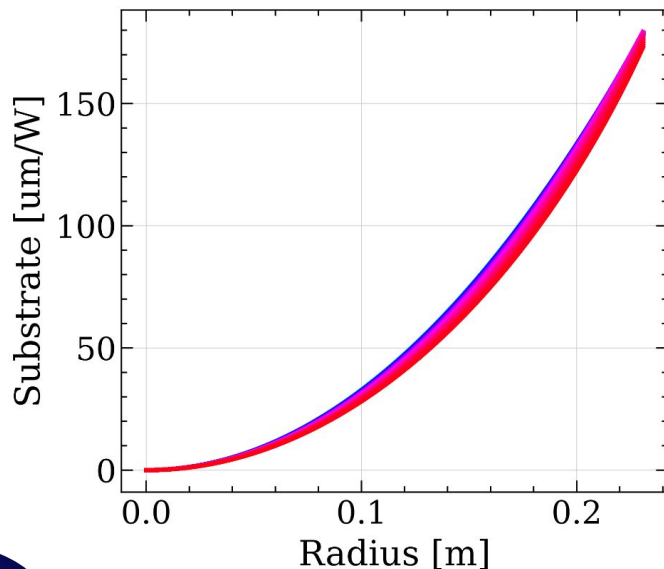
Actuation gain ratio for surface vs. substrate from RH have to match the defocus ratio due to self heating



Defocus ratio
SURF/Substrate
= **0.0767**

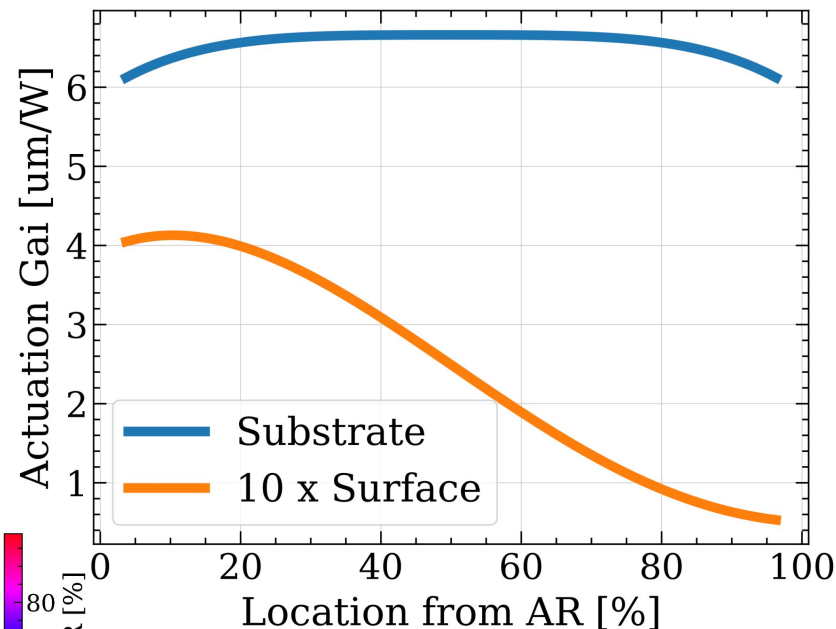
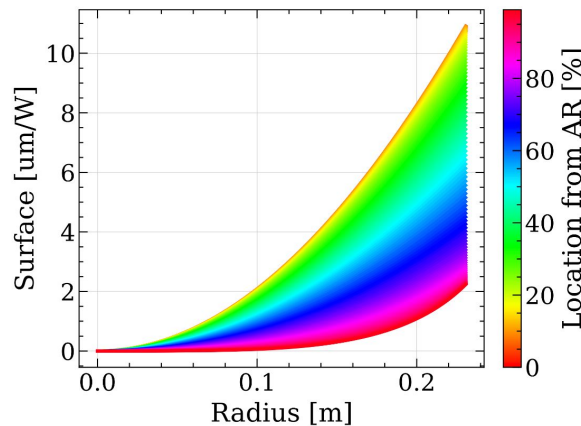
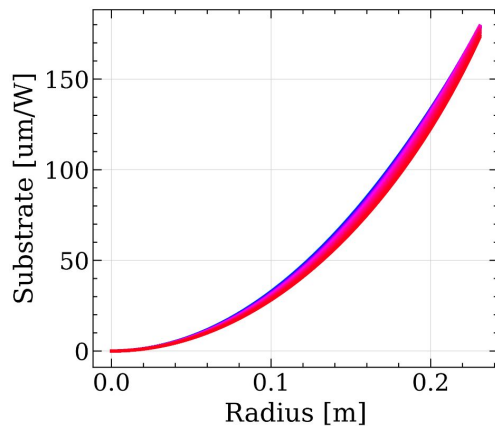
The curvature
actuation gain
ratio from RH
have to be close
to this number

Ring heater
location on the **surface**
and
substrate
actuation
gains



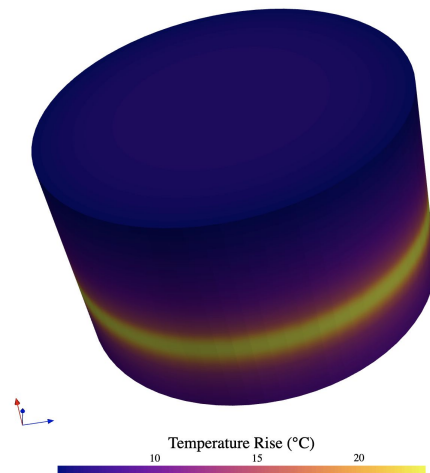
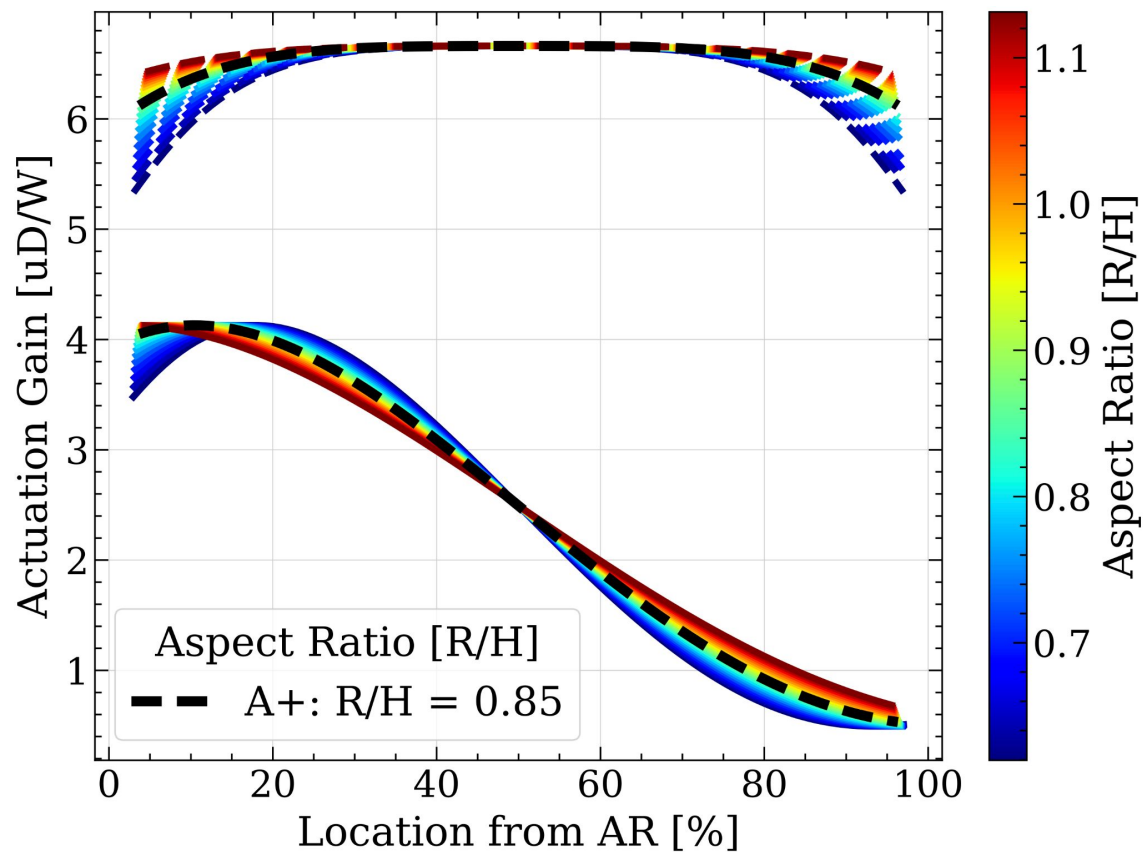
1. The substrate OPD is not sensitive to the RH location.
2. The surface OPD varies significantly. The closer to the AR, the larger the actuation gain.

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2. The surface OPD varies significantly. The closer to the AR, the larger the actuation gain.

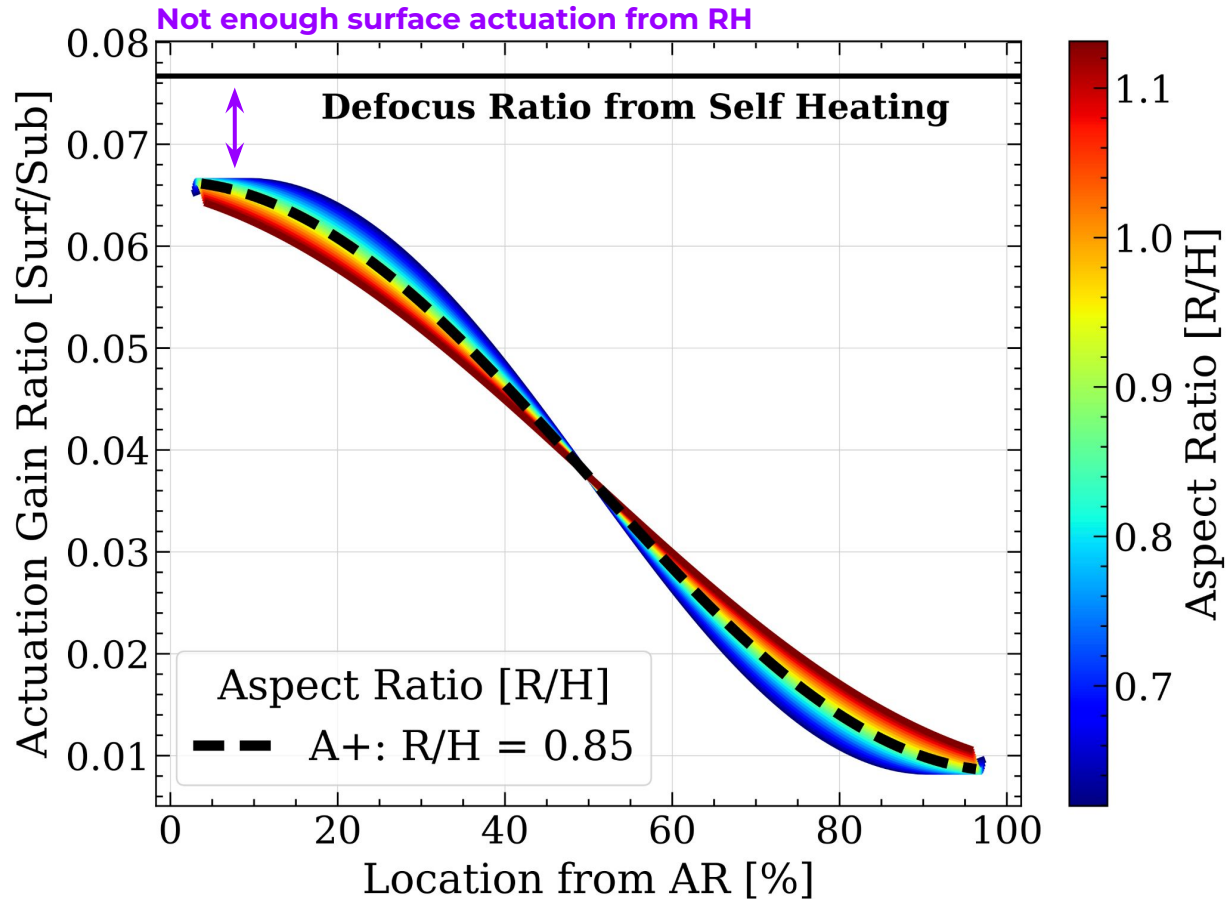


We need (*) even larger surface actuation gain.
Change the aspect ratio of the test mass?

* Slightly different results with beam size weighted quadratic fit from Tyler

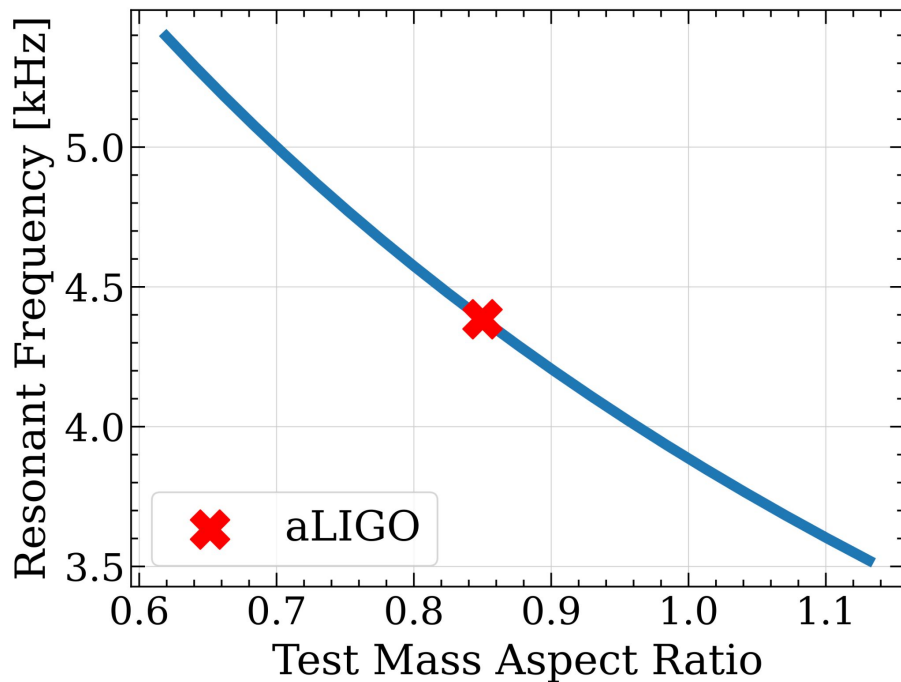


Allow the aspect ratio to change. The actuation gains vary.



1. The ratio of the actuation gain (surf./sub.) varies according to the RH location, and the aspect ratio.
2. But it is always smaller than the defocus ratio from self heating.

Resonant frequency vs. aspect ratio of the test mass (COMSOL)

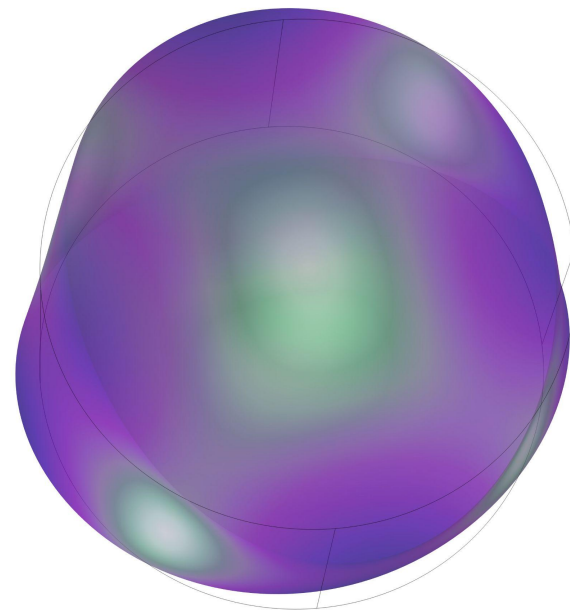


constant aspect ratio, these frequencies scale as $1/R$. For $\alpha \gtrsim 3$, they are well approximated by

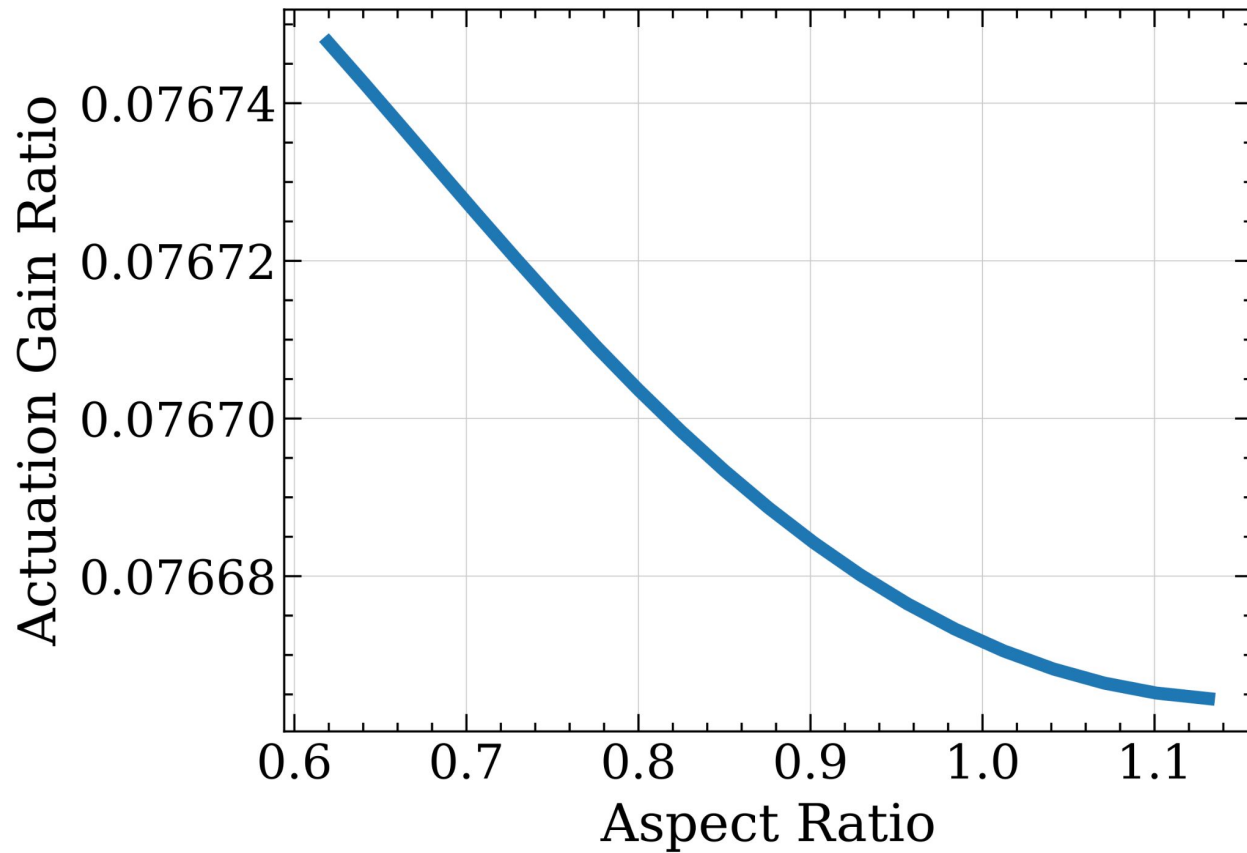
For BS-like optics only

$$f_{\text{butterfly}} = 7.27 \text{ kHz} \left(\frac{4}{\alpha} \right) \left(\frac{5 \text{ cm}}{R} \right) \quad (2a)$$

$$f_{\text{drumhead}} = 10.88 \text{ kHz} \left(\frac{4}{\alpha} \right) \left(\frac{5 \text{ cm}}{R} \right). \quad (2b)$$



Lowest mechanical resonance “butterfly” mode



The defocus ratio from self heating is not strongly affected by the aspect ratio of the test mass